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## **CHEMICAL ENGINEERING REFRESHER COURSE**

## **UNIT OPERATIONS 2 PART 2**

1.	Formation of large crystals is favo a. a low nucleation rate	red by	C	a high magma density		
	b. a high degree of supers	aturation	d.	a low magma density		
2.	A sphere having a diameter of 0.042 m is held in a small wind tunnel, where air at 37.8°C and 1.0 atm abs. and various velocities is forced past it, at this condition density is 1.137 kg/m³ and viscosity is 1.9 x 10 <sup>-5</sup> kg/m-s. Assuming Stokes' law, the force on the sphere for a velocity of 2.3 x 10 <sup>-4</sup> m/s is  a. 1.729 x 10 <sup>-9</sup> N					
	b. 1.831 x 10 <sup>-8</sup> N		d.	2.135 x 10 <sup>-9</sup> N		
3.	The wire diameter of a screen of r a. 0.0055 in b. 0.004 in	nesh size TBC (tensile bolting cloth) 94 is	s C. d.	0.0035 in 0.0026 in		
4.	A mixture of galena ( $\rho = 7500 \text{ kg/m}^3$ ) and silica ( $\rho = 2650 \text{ kg/m}^3$ ) having a size range between 0.025 mm to 0.08 mm is separated by elutriation using water. Assume the density and viscosity of water to be 1000 kg/m3 and 1.0 cp respectively. The velocity of water needed to obtain a pure galena product, assuming Stokes' law applies is					
	a. 0.06 m/s b. 0.045 m/s	119/41	c. d.	0.57 m/s 0.0056 m/s		
5.	The viscosity of ethyl benzene is _	cp at 60°C				
	a. 0.24		C.	0.14		
	b. 0.56		d.	0.44		
6.	An available crusher has been accepting hard rock with a volume-surface mean diameter of 0.069 m and providing a product with a volume-surface mean diameter of 5 x 10-3 m. The power required for crushing 10,000 kg/h of this specific rock is 6.35 kW. Assume that the mechanical efficiency of the unit will remain unchanged. The power consumption using Bond's law if the capacity were reduced to 9000 kg/h with the same feed characteristics but with a reduction in the volume surface mean diameter of the product to 4 x 10-3 m is					
	a. 7.35 kW		C.	6.64 kW		
	b. 7.0 kW		d.	8.64 kW		
7.	A mixture of particles in packed bed contains the following volume percent of particles and sizes: 15%, 10 mm; 25%, 20 mm 40%, 40 mm and 20%, 70 mm. The effective mean diameter, Dpm if the shape factor is 0.74 is					

d. 18.34 mm

a. 23.43 mm c. 12.38 mm

b. 16.81 mm

8.	sigma va process	alue of 7400 ft² the same brotl = 5 cm, r₁ = 2 cr	was computed, with a n, the largest tubular	a measured volume bowl centrifuge av	etric flow rate of 0.1 vailable has the fo	ntation broth. At the operating cor 11 gal/min. For the commercial pla llowing characteristics: bowl speed eory, the volumetric flow rate of thi	nt that wil I = 15000
	' а. b.	0.92 gal/min 0.37 gal/min			c. d.	0.47 gal/min 0.59 gal/min	
9.	What is characte a. b.					following specifications and per in and typical motor size = 7.5 Hp? 24 in 10 in	
10.	equation conveying	n 21-92 page 2 ng rate of 7500	1-46 Perry ChE HB kg/h through a 100 m	9the edition to calo	culate the choking a diameter. The co	olids can no longer be carried upvoledity of a 10-micron particle wonveying gas is air at 22°C and 150 fighther. The choking velocity is 4.2 m/s 1.57 m/s	ith a solid
11.			equipment that is us size distribution is	ed in chemical indu	ustry for processing c. d.	p brittle-heat sensitive materials into Pan Crushers Tumbling Mill	o very fine
12.		liquid-liquid ph				sion path lengths and increasing t put with very low liquid residence ti Centrifugal extractor Static Extraction Column	
13.	Zinc is to be recovered from an ore containing zinc sulfide. The ore is first roasted with oxygen to produce zinc oxide, which is then leached with aqueous sulfuric acid to produce water soluble zinc sulfate and an insoluble, worthless residue called gangue. The decanted sludge of 20,000 kg/h contains 5 weight % water, 10 weight % zinc sulfate and the balance as gangue. This sludge is to be washed with water in a continuous countercurrent washing system to produce an extract, called a strong solution, of 10 weight % zinc sulfate in water with a 98 % recovery of the zinc sulfate. Assume that the underflow from each washing stage contains, by weight, two parts of water (sulfate-free basis) per part of gangue, the number of stages required is a. 4						
	b.	6	1	107	d.	10	
14.	With the a. b.	lowering of equincreases remains the s		a given temperature	e, the amount of ad c. d.	sorbate on adsorbent decreases may increase or decrease	
15.				<sup>=</sup> of a particle with a		5.0 and diameter of 100 microns is 0.081 0.028	ft/s
16.	involves solvent.	hydrogen bond Its partition ratio 0.65		example is the extra	action of citric acid	ity between the feed and extraction from water using 1-butoxy-2-properties.	
	b.	0.40			d.	0.20	

17. The following equilibrium relationship was obtained during the treatment of an aqueous solution of a valuable solute by decolorizing carbon for removal of coloring impurities:  $Y = 8.91 \times 10^{-5} X^{1.66}$ 

where X = adsorbate concentration per kg of carbon and Y = equilibrium color units per kg of solution measured on an arbitrary scale proportional to the concentration of the colored impurity.

It is proposed to reduce the color of the solution to 20% of its original value of 9.0. The quantity of fresh carbon required per 100 kg of the solution in single stage operation is

a. 4.18 kg c. 7.2 kg b. 5.6 kg d. 1.84 kg

18. The average work index of CaSO<sub>4</sub> 2H<sub>2</sub>O in kWh/ton is

a. 13.11 c. 25.17 b. 8.16 d. 45.03

19. A crusher is fed with limestone having particles of 2.0 cm median equivalent diameter and discharges a product consisting of particles of 0.50 cm median equivalent diameter. The feed particles can be considered very coarse and so Kick's law would be the most appropriate. The equipment operates at a capacity of 1.2 x 10<sup>4</sup> kg/h consuming a power of 10 Hp. If the requirements of the process demand a finer size of the product (0.4 cm of median equivalent diameter) decreasing the capacity to 1.0 x 10<sup>4</sup> kg/h, the theoretical power consumption under the new conditions is

a. 5.3 kW b. 7.2 kW c. 6.2 kW d. 8.6 kW

20. The solubility of strontium acetate in water at 0°C is \_\_\_\_parts per 100 parts water.

a. 53.5 b. 33

21. For a solid spherical particle of 0.80 mm in diameter and a density of 2600 kg/m3 that is immersed in a fluid of density 1200 kg/m3 and a viscosity of one centipoise, the unhindered terminal velocity is

a. 0.975 m/s b. 0.0975 m/s d. 0.0579 m/s

22. The mutual solubility of two salts can be plotted on the X and Y axes with temperatures as isotherm lines. If both solid-phase KCl and NaCl are present, the solution composition at equilibrium can only be represented by the invariant point (at constant pressure). The solubility ratios in parts per 100 parts water of KCl and NaCl at 40°C are:

a. 34.3 and 27
b. 20.4 and 28.4
c. 35 and 27.5
d. 22.6 and 31.4

23. The average pore diameter and surface area of polyacrylic ester for purification of pulping wastewaters and antibiotics recovery are

24. It is desired to recover lead from an ore containing 10% lead sulfide (PbS) and the balance assumed to be silica, 500 tons of ore being treated per 24 hr-day. It is assumed that the concentrate from a single cell is of acceptable purity but the tailings are to be retreated in scavenger cells with return of scavenger concentrate to the rougher. Laboratory findings indicate that if the water to solids ratio L/S = 2.0 and the contact time is 8 min in the rougher and L/S = 4.0 for 15 min in scavenger with mechanically agitated machines of the Denver type. The following compositions will be found for the various products:

	PbS	SiO <sub>2</sub>
Feed	10%	90%
Final Concentrate	80%	20%
Rougher Tailings	2%	98%
Scavenger Concentrate	11%	89%
Final Tailings	0.5%	99.5%

The densities of PbS and SiO<sub>2</sub> are 7.5 and 2.65 g/cc respectively.

The volume needed in the scavenger is

a.  $750 \, \text{ft}^3$  c.  $680 \, \text{ft}^3$  b.  $570 \, \text{ft}^3$  d.  $840 \, \text{ft}^3$ 

- 25. The step in mineral ore flotation where low concentrated product is returned for repeated flotation.
  - scavenger concentrate scavenger flotation

rougher flotation final concentrate

- END -

